

EE533-12

note: no class - Lecture 11

example: $f = 1 \text{ MHz} \Rightarrow \lambda = 300 \text{ m}$ Let $L = 1 \text{ m}$ (old style car ant)

$$R_r = 80\pi^2 \left| \frac{1}{300} \right|^2 = 0.00876 \Omega \text{ (for uniform I } \text{---} \text{---} \text{---})$$

$$R_r = 20\pi^2 \left| \frac{1 \text{ m}}{300 \text{ m}} \right|^2 = 0.00219 \Omega \text{ (for Linear I } \text{---} \text{---})$$

$$R_s = \sqrt{\frac{\mu_0}{2\sigma}} = 2.63 \times 10^{-4}$$

$$R_\Omega = 0.103 \Omega (\text{---})$$

$$R_\Omega = 0.0344 \Omega (\text{---})$$

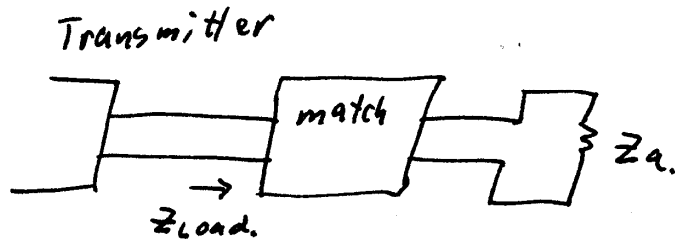
$$\eta = 7.8\%$$

$$\eta = 6\%$$

$\Rightarrow$ we lose more than 90% of the power to heat! (even if we could match a T Line to the antenna!)

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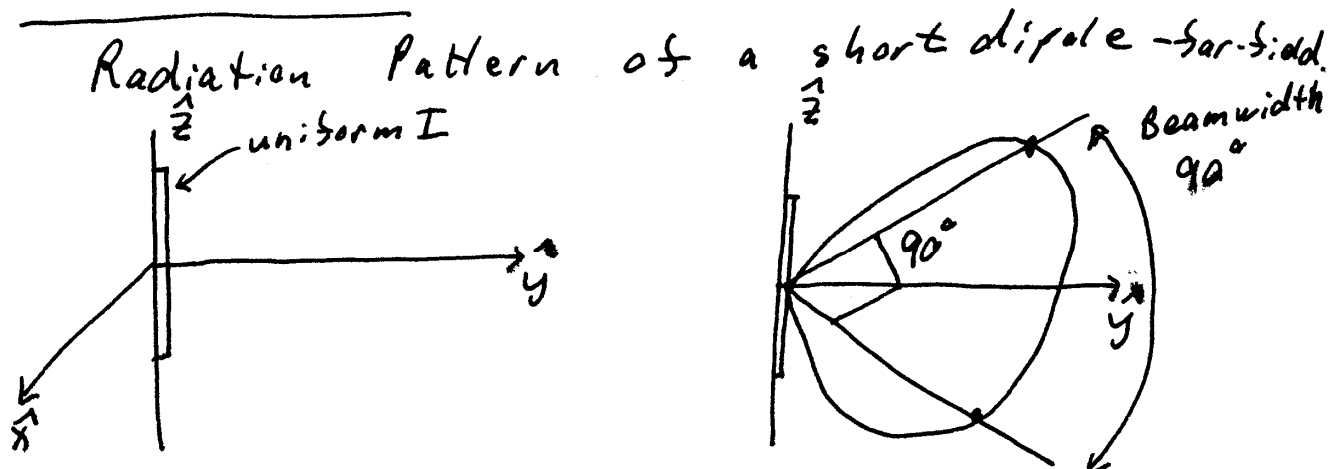
when Z_a is very small it is very difficult to design a low loss matching network, $\Rightarrow$ AM car antennas use a partial match & live with the very low efficiency!

To increase η we must increase the antenna size $\Rightarrow \approx \lambda/2$ if possible.

example:

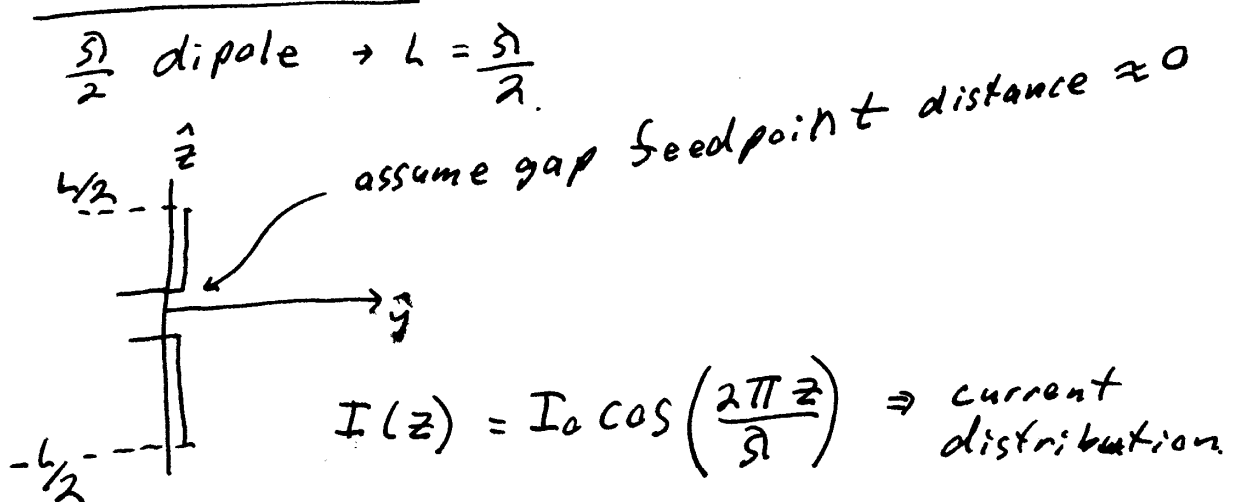
Cell phone Antenna $f \approx 1\text{GHz}$

$\lambda = .3\text{m} = 30\text{cm} \Rightarrow \eta \approx 99\%$ are possible.



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 $\hat{x}-\hat{y}$ plane : omnidirectional radiation
$$\left. \begin{array}{l} \hat{y}-\hat{z} \\ \hat{x}-\hat{z} \end{array} \right\} \text{ plane; Beamwidth} = 90^\circ \quad \text{note: for Both } \left\{ \begin{array}{l} \text{---} \text{Z} \text{---} I \\ \text{---} \text{Z} \text{---} I \end{array} \right.$$
the directivity $D = \frac{3}{2} = 1.76 \text{ dB}$; (see text for details) $\frac{\lambda}{2}$ dipole $\rightarrow L = \frac{\lambda}{2}$ 

$$I(z) = I_0 \cos\left(\frac{2\pi z}{\lambda}\right) \Rightarrow \text{current distribution}$$

$$E_\phi = 0$$

$$E_\theta = j\omega\mu \frac{2I_0}{k} \frac{e^{-jkr}}{4\pi r} \frac{\cos\left[\frac{\pi}{2}\cos\theta\right]}{\sin\theta}$$

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The normalized field $F(\theta) = \frac{\cos\left[\frac{\pi}{2} \cos\theta\right]}{\sin\theta}$

$$0 = 1.64 = 2.15 \text{ dB}$$

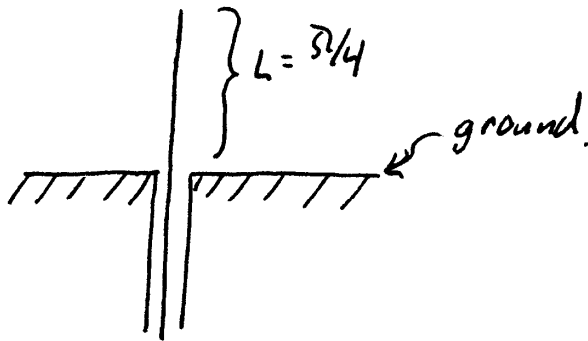
$R_r = 73\Omega$ fixed value.

$R_\Omega = 7.7\Omega$ for copper.

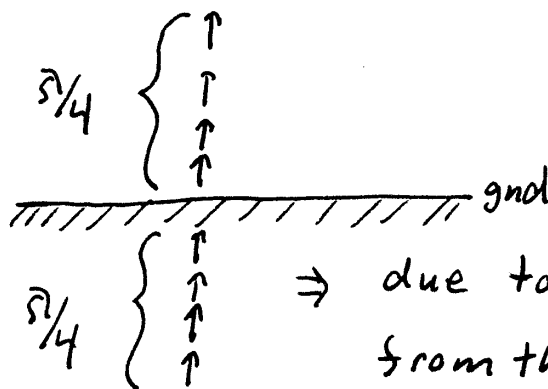
then $\eta = 90\%$!

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the monopole $\Rightarrow$ special case of dipole.



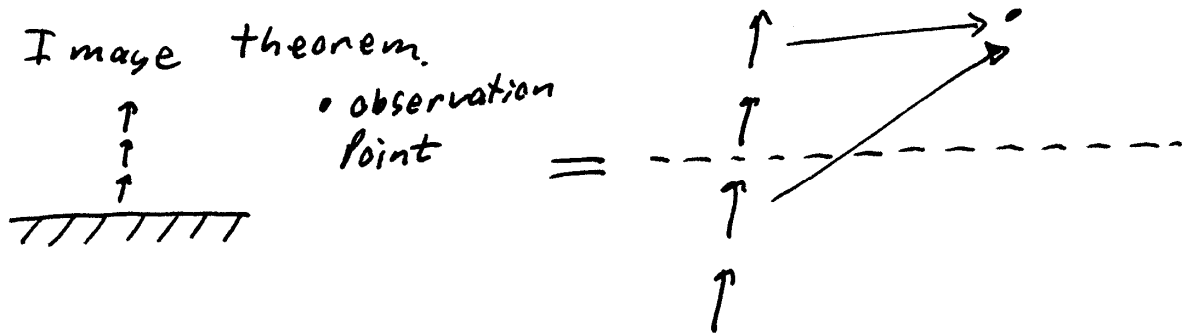
Radiation is from the current on the wire and the induced current on the ground plane.



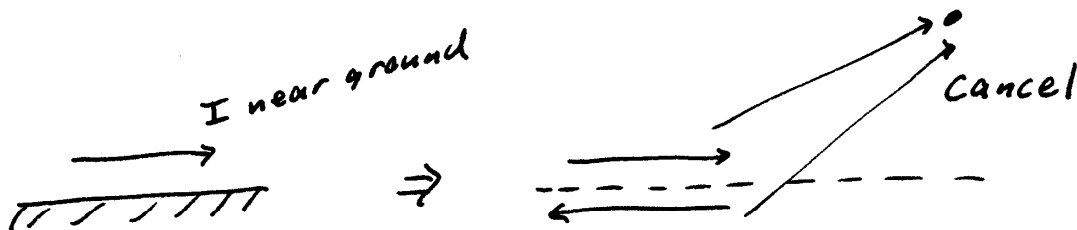
by image theory
(see section 4.71 text)

$\Rightarrow$ due to the image (i.e. the contribution from the induced current on the ground plane)

$\frac{\eta}{4}$ + gnd plane $\approx$ a $\frac{\eta}{2}$ dipole.



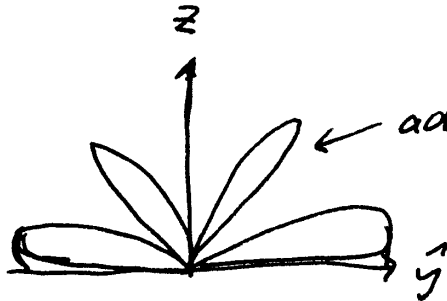
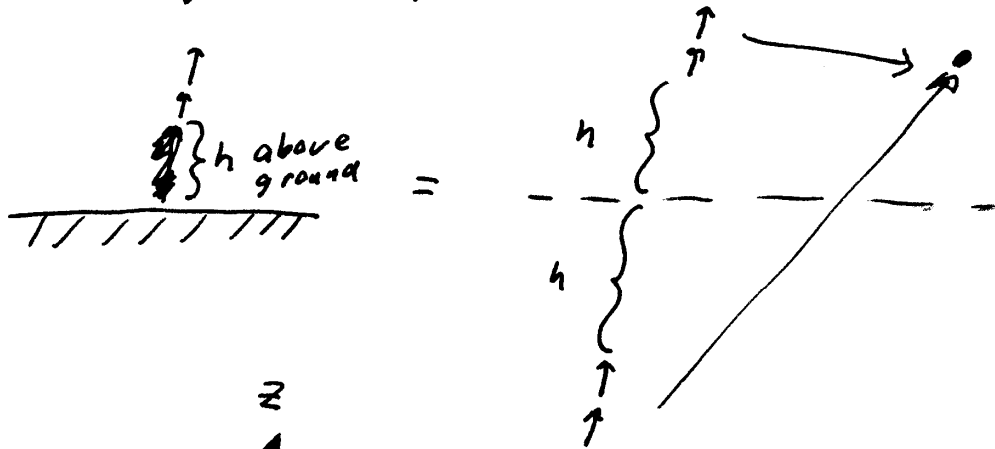
note for current distributions near the ground, this only works when I is $\perp$ to the ground.



this is an example of microstrip line on a PCB. the line is not radiating. but is transporting E+M power along the transmission line.

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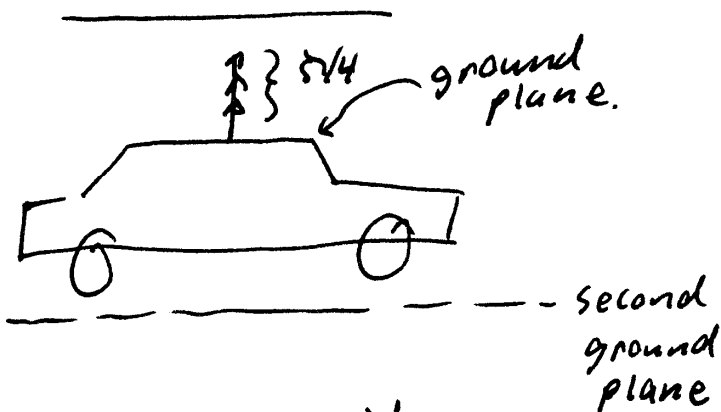
as the antenna is placed higher above the ground, additional lobes appear and the gain drops.



additional lobes as h increases.

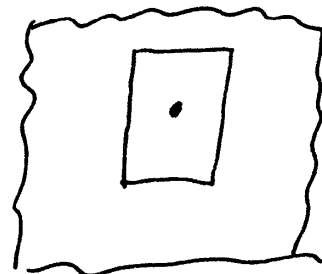
see fig 4.15 in text.

$$\text{number of lobes} \approx \frac{2h}{\lambda} + 1$$



so some side lobes are possible depending on λ .

Top view.



example of stepped gnd plane.

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Directivity of $\frac{3}{4}$ on ground:

$$D_{3/4} = \frac{\Omega}{4} + \text{gnd directivity} = 2 D_{3/2}$$

this is because the power is radiated only 180° in elevation plane.
 (Dot $\frac{\Omega}{2}$ antenna.)

from before, $D_{3/2} = 1.64 = 2.15 \text{ dBi}$

$$D_{3/4} = 2 D_{3/2} = 3.28 = 5.16 \text{ dBi!}$$

this is substantial

from Text: $Z_a|_{3/2} = 73 + j42.5$ (4-93 txt)

$$Z_a|_{\frac{\Omega}{4}} = \frac{Z_a|_{3/2}}{2} = 36.5 + j21.25 \quad (4-106 \text{ txt})$$

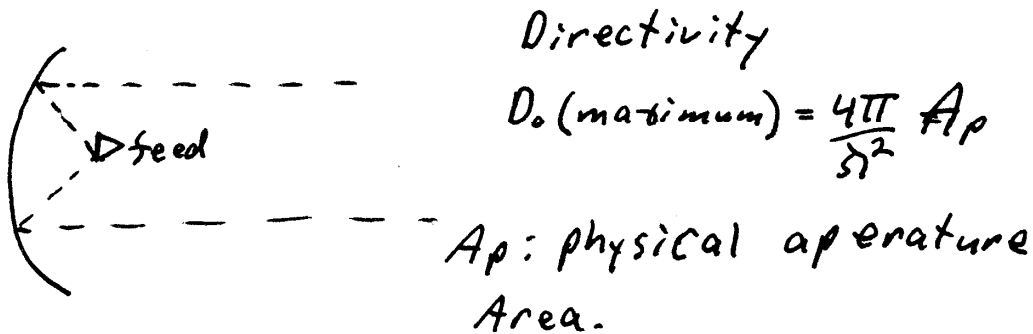
see Table 4.2 in Text for
Summary of dipole in Far Field.

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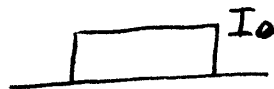
Gain $\Rightarrow G = D \cdot \eta_e$ where $\eta_e < 1$ is the antenna efficiency

for a dipole antenna: $\eta_e < 10\%$ short dipole
 $\eta_e > 90\%$ $\frac{\lambda}{2}$ dipole.

High gain antennas are usually a reflector type:



D_o is only achieved with uniform field distribution.



$G = \frac{4\pi}{\Omega^2} A_e$ A_e is the "effective" area.
 this corrects for the non uniform field dist over the physical aperture.

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$$A_e < A_p$$

$$A_e = \epsilon_e A_p \quad \epsilon_e = \text{Aperture efficiency}$$

$$\text{so } G = \left(\frac{4\pi}{\lambda^2} A_p \right) \epsilon_e \quad \text{for dish antennas.}$$

$\epsilon_e \approx 55\%$ including feed point coupling.

gain increase using pattern multiplication.
 the gain of a simple antenna is usually small. this is ok for some applications, but what about where we want higher gain? (ex: point to point fixed Link.)

One method is to use an array of simple antennas to increase $A_e \Rightarrow$ which will increase G .

